

Plasticity Equations Recap :

$$\Psi = \Psi(\epsilon, \epsilon_p, \alpha) = \underbrace{\Psi_e(\epsilon_e)}_{\epsilon - \epsilon_p} + \Psi_h(\alpha)$$

$$D = \sigma : \dot{\epsilon}_p + A \dot{\alpha} \geq 0, \quad \sigma = \frac{\partial \Psi}{\partial \epsilon_e} = - \frac{\partial \Psi}{\partial \epsilon_p}$$

$$A = - \frac{\partial \Psi}{\partial \alpha}$$

$$E = \{(\sigma, A) \mid f(A, \sigma) \leq 0\}$$

plastic multiplier

yield function + elastic region

$$\dot{\epsilon}_p = \dot{\gamma} \frac{\partial g}{\partial \sigma}, \quad \dot{\alpha} = \dot{\gamma} \frac{\partial g}{\partial A}$$

g = plastic potential
 $g = f$ associative flow

$$\dot{\gamma} \geq 0, \quad f \leq 0, \quad \dot{\gamma} f = 0 \quad \text{KKT}$$

$$\begin{aligned} \dot{\gamma} > 0 &\leftrightarrow f = 0 \\ \dot{\gamma} = 0 &\leftrightarrow f < 0 \end{aligned}$$

$$\dot{\gamma} = \frac{\frac{\partial f}{\partial \sigma} : \mathbb{C} : \dot{\epsilon}}{\frac{\partial f}{\partial \sigma} : \mathbb{C} : \frac{\partial g}{\partial \sigma} + H}$$

from consistency condition $\dot{f} = 0$

$$\frac{\partial f}{\partial A} \frac{\partial^2 \Psi}{\partial \alpha^2} \frac{\partial g}{\partial A}$$

4. J₂ Plasticity (von Mises 1913)

Plastic deformation occurs due to the deviatoric part of stress:

$$\boldsymbol{\sigma} = \underbrace{\frac{\text{tr } \boldsymbol{\sigma}}{3} \mathbf{1}}_{\text{mean stress}} + \underbrace{\boldsymbol{S}}_{\text{deviatoric stress}}, \quad \text{tr } \boldsymbol{S} = 0$$

$$|\boldsymbol{S}| \equiv \sqrt{\boldsymbol{S} : \boldsymbol{S}} \equiv \sqrt{2 J_2} \rightarrow J_2 = \frac{1}{2} \boldsymbol{S} : \boldsymbol{S}$$

$$\boldsymbol{Q} = \frac{\boldsymbol{S}}{|\boldsymbol{S}|}, \quad |\boldsymbol{Q}| = 1, \quad \text{tr } \boldsymbol{Q} = 0$$

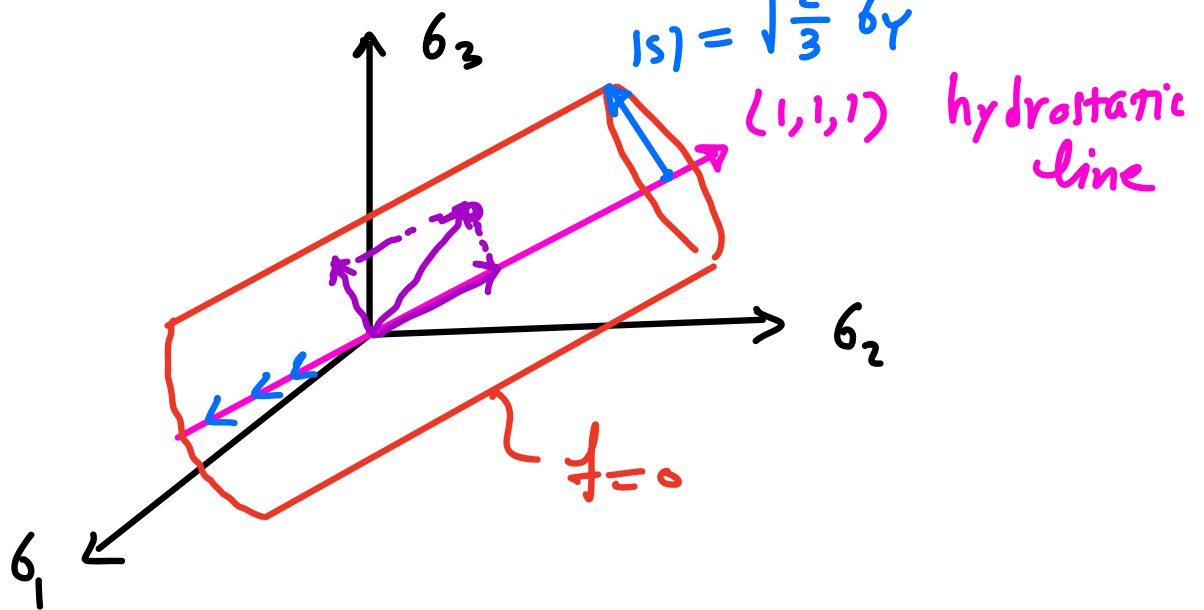
Yield surface/function

$$\mathcal{F}(\boldsymbol{\sigma}, A) = \sqrt{3 J_2} - (\underbrace{\sigma_y}_{\text{yield stress}} - A) \leq 0$$

$\dot{\boldsymbol{\epsilon}} = \dot{\boldsymbol{\epsilon}}^p$ associative flow

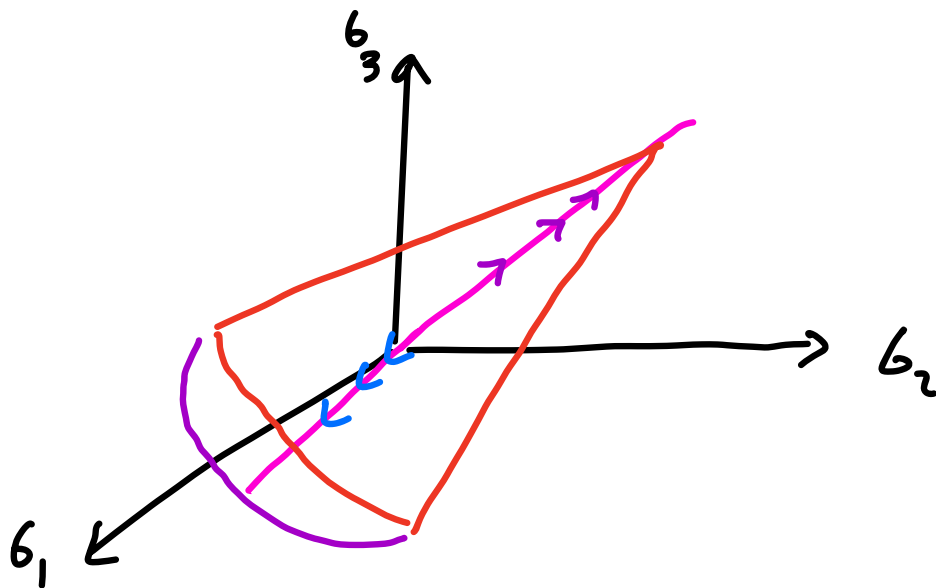
$$\underbrace{\sqrt{3 J_2}}_{\sigma_y} = \sqrt{3} \frac{|\boldsymbol{S}|}{\sqrt{2}} = \sqrt{\frac{3}{2}} |\boldsymbol{S}|$$

Metal :



$$\sigma = \sigma_m (1,1,1) + \underline{\underline{(s_1, s_2, s_3)}}$$

Other :



Ex: Uniaxial tension & Pure shear (1D)

tension :

$$\sigma = \begin{pmatrix} \sigma_1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}, \quad \sigma_m = \frac{\text{tr } \sigma}{3} = \frac{\sigma_1}{3}$$

$$s = \sigma - \sigma_m \mathbf{1} = \begin{pmatrix} \frac{2}{3} \sigma_1 & 0 & 0 \\ 0 & -\frac{\sigma_1}{3} & 0 \\ 0 & 0 & -\frac{\sigma_1}{3} \end{pmatrix}$$

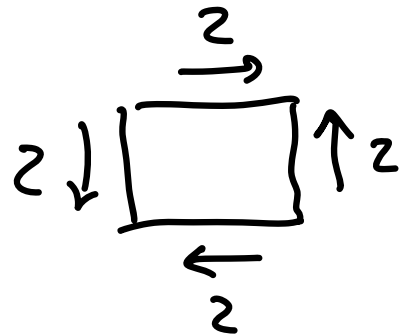
$$\begin{aligned} J_2 &= \frac{1}{2} S:S = \frac{1}{2} \left(\frac{4}{9} b_1^2 + \frac{b_1^2}{9} + \frac{b_1^2}{9} \right) \\ &= \frac{1}{2} \frac{6}{9} b_1^2 = \frac{1}{3} b_1^2 \end{aligned}$$

$$\rightarrow \boxed{b_1 = \sqrt{3 J_2} = b_Y} \quad b_1 \leftarrow \text{---} \rightarrow b_1$$

$\phi = 0$

Shear :

$$b = \begin{pmatrix} 0 & 2 & 0 \\ 2 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$



$$S = b, \quad J_2 = \frac{1}{2} S:S = \frac{1}{2} (\tau^2 + \tau^2)$$

$$\rightarrow J_2 = \tau^2 \rightarrow \tau_Y = \frac{\sqrt{J_2} \sqrt{3}}{\sqrt{3}} = \frac{b_Y}{\sqrt{3}}$$

$$\boxed{\tau_Y = \frac{b_Y}{\sqrt{3}}}$$

Flow rule :

$$\dot{\epsilon}_p = \gamma \frac{\partial f}{\partial b}, \quad \dot{\alpha} = \gamma \frac{\partial f}{\partial A} = 1$$

$$\sqrt{\frac{3}{2}} Q''$$

$$Q = \frac{s}{|s|}, |Q|=1$$

$$f(b, A) = \sqrt{3 J_2} - (b_y - \underline{A})$$

$$\rightarrow \dot{\epsilon}_p = \dot{\gamma} \sqrt{\frac{3}{2}} Q, \quad \dot{\alpha} = \dot{\gamma}$$

Plastic Multiplier:

$$\epsilon = \epsilon_v 1 + e$$

deviatoric

$$\dot{\gamma} = \frac{\sqrt{6} \mu (Q : \dot{e})}{3\mu + H}$$

shear modulus (at C)

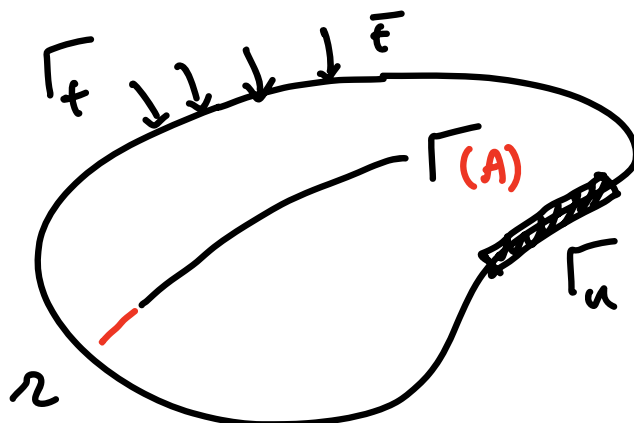
$$\frac{\partial^2 \psi_h}{\partial \alpha^2}$$

Fracture & Phase-field method

1. Griffith's view of fracture (1921)

energy released

= Cost of creating the crack



Def. Potential energy & Energy release rate

$$\Pi(A) \equiv \int_{\Omega \setminus \Gamma(A)} \psi(\epsilon) - \int_{\Omega} b \cdot u - \int_{\Gamma_t} \bar{t} \cdot u$$

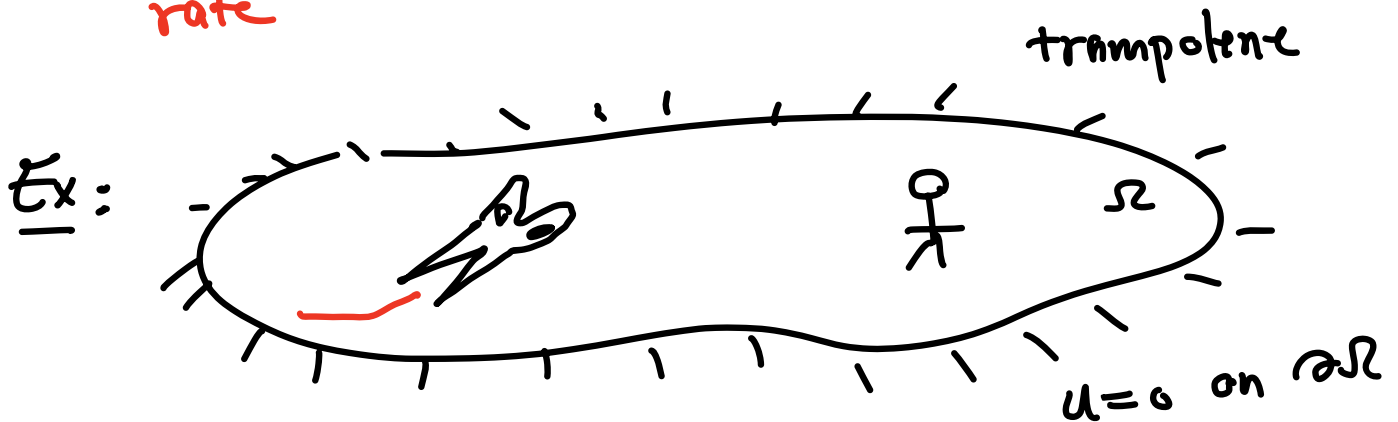
Equilibrium

$u, \epsilon =$ solution
to equilibrium
in momentum

$A =$ crack area
trajectory is known
 $\Leftrightarrow$ parameterize $\Gamma(A)$

$$G \equiv - \frac{d\Pi}{dA}$$

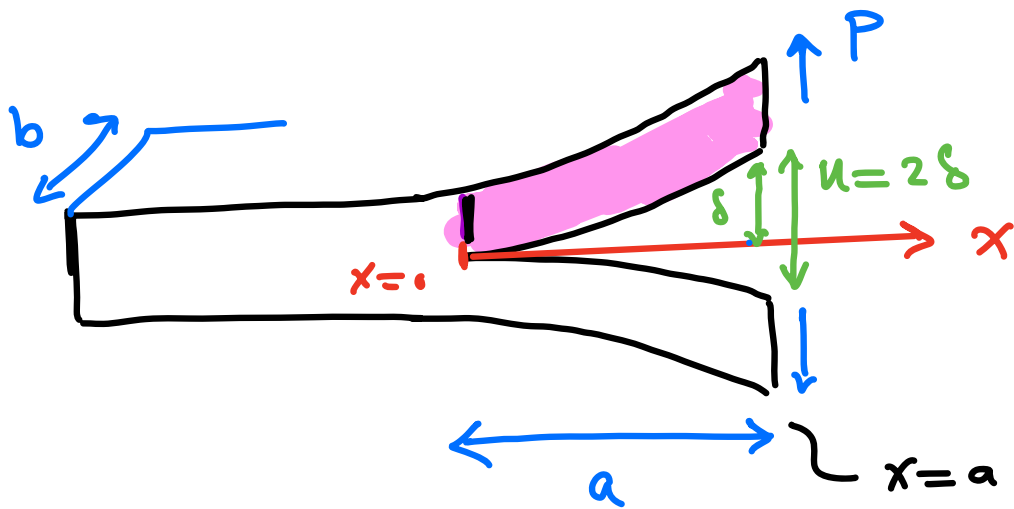
Energy release
rate



$$\Pi(A) = \int_{\Omega \setminus \Gamma(A)} \psi dV = U(A)$$

$$G = - \frac{dU}{dA}$$

Ex: Double Cantilever Beam (DCB)



① Load Control:

$$EI \omega'''' = 0, \quad \text{BCs} = \text{4th order.}$$

$$\omega(x) = \frac{P}{6EI} (3ax^2 - x^3)$$

at $x=a$

$$\rightarrow \delta = \omega(a) = \frac{Pa^3}{3EI}$$

$$\rightarrow \boxed{u = 2\delta = \frac{2Pa^3}{3EI}}$$

$$\rightarrow \boxed{u = C(A) P}$$

$$C(A) = \frac{2a^3}{3EI}$$

Compliance

$$\boxed{\omega(0) = 0, \quad \omega'(0) = 0}$$

clamped

$$M(a) = 0, \quad V(a) = P$$

$$EI \omega''(a)$$

$$-M'(a)$$

$$-EI \omega'''(a)$$

$$\boxed{\omega''(a) = 0}$$

$$\boxed{-EI \omega'''(a) = P}$$

$$\Pi = \cancel{U} - \cancel{W_{ext}} \xrightarrow{A=ba} \Pi = -\frac{Pu}{2}$$

$$\frac{1}{2} \sum_i P_i u_i = \frac{Pu}{2}$$

$$\rightarrow \boxed{\Pi(\underline{A}) = -C(\underline{A}) \frac{P^2}{2}}$$

$$G = -\frac{d\Pi}{dA} = \frac{dC}{dA} \frac{P^2}{2}$$

$$\rightarrow \boxed{G = \frac{P^2 a^2}{bEI}}$$

foreshadowing

$$G \leq G_c$$

$G = G_c$ crack grows

NB. $a \rightarrow 0, G \rightarrow 0$

$$G \propto a^2$$

②

Displacement Control : $P = \frac{u}{C(A)}$

$$\boxed{G = \frac{9EI \circledast u^2}{4ba^4}}$$

$$G \propto \frac{1}{a^4}$$

$a \rightarrow 0, G \rightarrow \infty$

Griffith's Criterion for stable fracture

$$\dot{A} \geq 0, \quad G - G_c \leq 0, \quad (G - G_c) \dot{A} = 0$$

fracture toughness
(material property)

these are KKT conditions (w/ a threshold G_c).

Meaning:

- ① if $G < G_c \Rightarrow \dot{A} = 0$ crack does not grow
- ② if $G = G_c \Rightarrow \dot{A} > 0$ stable crack growth
- ③ if $G > G_c \Rightarrow$ Inadmissible (crack growth is unstable)

Dissipation inequality is satisfied:

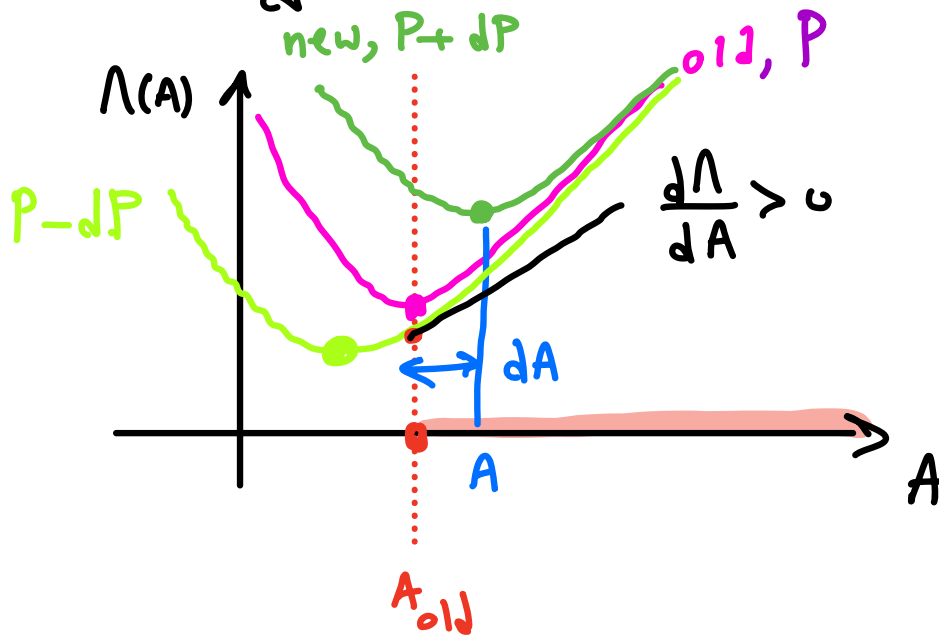
$$\mathcal{D} = \underbrace{G}_F \underbrace{\dot{A}}_{\dot{\gamma}} = \underbrace{G_c}_{>0} \underbrace{\dot{A}}_{\geq 0} \geq 0$$

Griffith as energy minimization

$$\min_{A \geq A_{old}} \Lambda(A), \quad \Lambda(A) \equiv \Pi(A) + G_c A$$

↓
realize "A" is the minimizer

This is equivalent to KKT (Caveat!):



loading

$$\textcircled{1} \quad \frac{d\Lambda}{dA} = \underbrace{\frac{d\Pi}{dA}}_{-G} + G_c = -G + G_c = 0$$

→ $G = G_c$ crack grows stably

unloading

$$\textcircled{2} \quad \frac{d\Lambda}{dA} = -G + G_c > 0 \rightarrow G < G_c$$

crack stays frozen

Key problem : Above picture requires $\Gamma(A)$ to be parameterized
 $\equiv$ crack trajectory is known

Generalizing to arbitrary crack trajectory :

$$\Lambda[u, \Gamma] = \int_{\Omega \setminus \Gamma} \psi dv - \int_{\Omega} b \cdot u - \int_{\Gamma} \bar{t} \cdot u + G_c \int_{\Gamma} |d\Gamma|$$

and

$$\min_{\substack{u \\ \Gamma \geq \Gamma_{old}}} \Lambda[u, \Gamma] = \min_{\Gamma \geq \Gamma_{old}} \min_u \Lambda[u, \Gamma]$$

↘ unconstrained

$$= \min_{\substack{\Gamma \geq \Gamma_{old} \\ A \geq A_{old}}} \Lambda[u_{eq}^{(A)}, \Gamma^{(A)}]$$

$A \geq A_{old}$

if crack path were known

The minimization seeks a global min.

(KKT $\iff$ local search around A_{old})

problem: nucleation Not Captured

Ex: Crack Nucleation in DCB

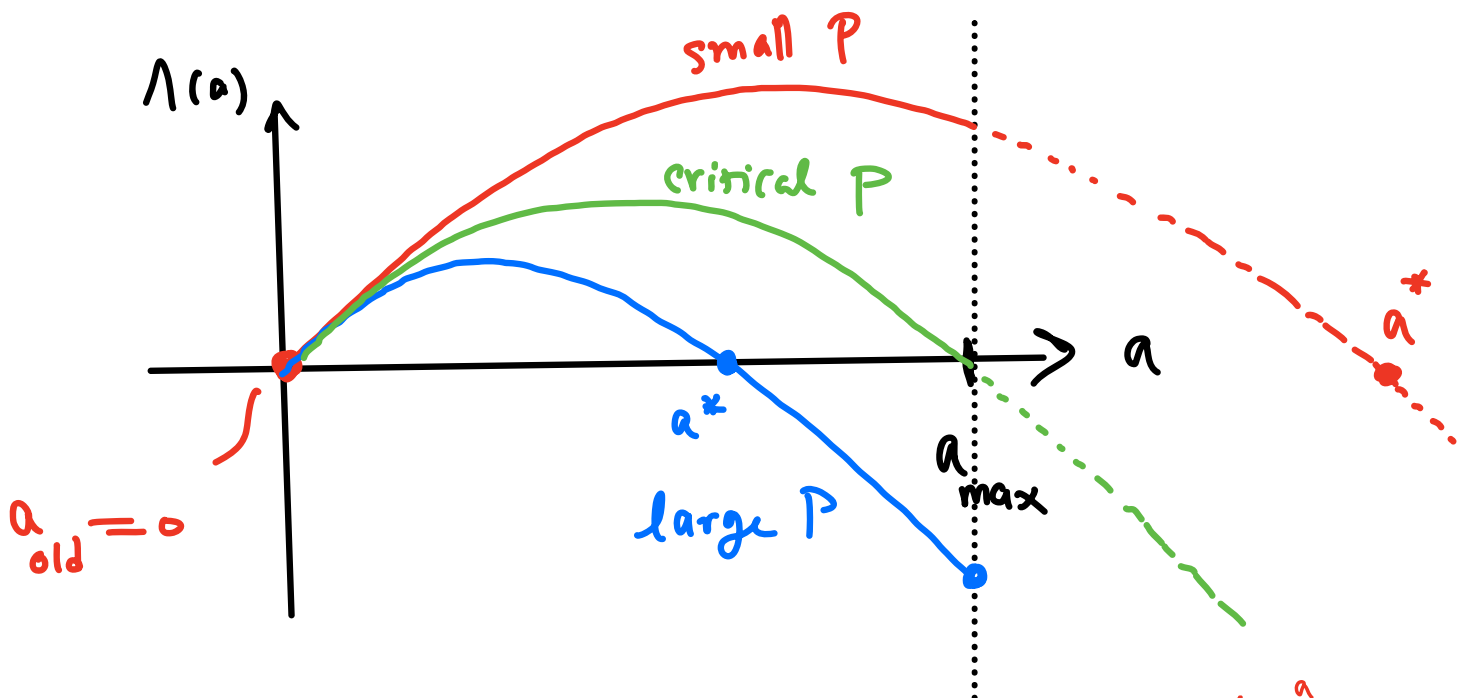
① Load Control

$$\Lambda = \Pi + G_c A$$

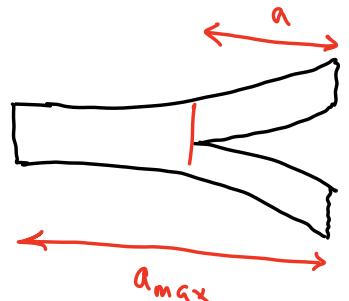
$$\rightarrow \Lambda(a) = -\frac{P^2 a^3}{3EI} + G_c b a$$

Suppose an intact initial state ($a=0$)

notice $\Lambda(0) = 0$.



- small $P \rightarrow a=0$ minimizer
- large $P \rightarrow a=a_{\max}$ minimizer

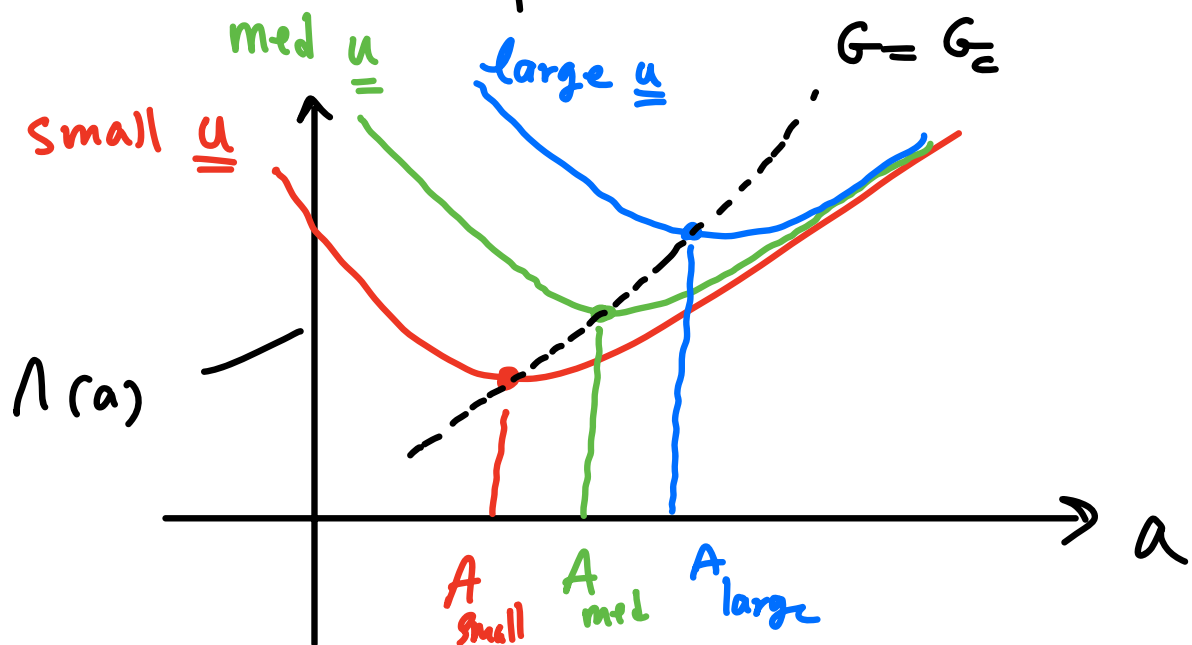


For small perturbations around P_{crit} , $\underline{a}$ goes from $\underline{0}$ to $\underline{a_{max}}$. $\Rightarrow$ unstable crack growth.

NB: $a \rightarrow 0$, $G \rightarrow 0 \Rightarrow$ local search predicts no crack
 $\frac{1}{2} G < G_c$

② Displacement Control

$$\Lambda(a) = \frac{3EI u^2}{4 a^3} + G_c b a$$



minima

Continuous charge

$$a_{eq} = \left(\frac{9EI u^2}{4b G_c} \right)^{\frac{1}{4}} \propto \sqrt{u}$$

2. Phase-field model of fracture

minimizing over $\underline{\Gamma}$ (Crack set) is hard,
but minimizing over a field (damage var)
is easy.

$$\Lambda[u, \Gamma] = \dots + G_c |\Gamma| \stackrel{A}{=}$$

Regularizing (replacing) the $G_c |\Gamma|$ term:

AT₂ = Ambrosio - Tortorelli

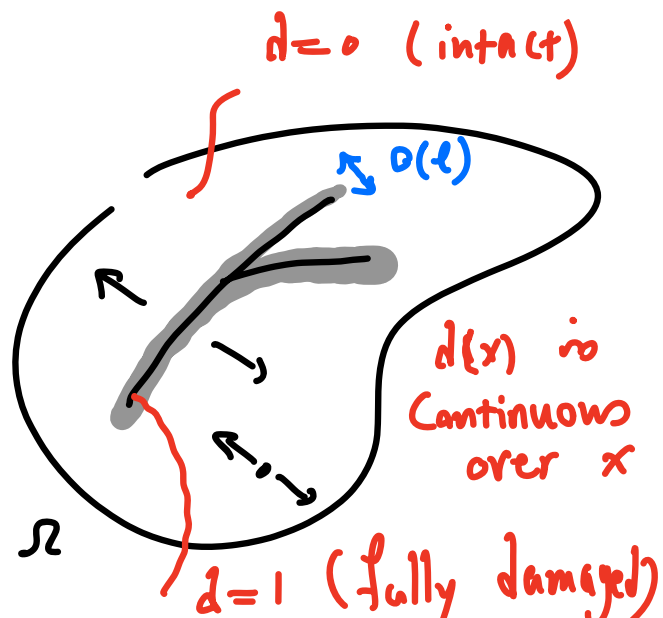
$$|\Gamma| \simeq \int_{\Omega} \gamma \, dV, \quad \gamma(d, |\nabla d|) = \frac{d^2}{2\ell} + \frac{\ell}{2} |\nabla d|^2$$

crack density function
length parameter

Reality (sharp)



$\simeq$



As $d \rightarrow 0$, the sharp crack is recovered.

Degradation Function

stored elastic energy density of intact

$$\Psi(\epsilon, d) = g(d) \Psi_0(\epsilon) \quad , \quad \Psi_0(\epsilon) = \frac{1}{2} \epsilon : \mathbb{C} : \epsilon$$

degradation function

$$g(d) = (1-d)^2$$

$$\sigma = \frac{\partial \Psi}{\partial \epsilon} = g(d) \frac{\partial \Psi_0}{\partial \epsilon} = \underline{g(d)} \mathbb{C} : \epsilon$$

$$g(0) = 1 \quad , \quad g(1) = 0 \quad , \quad g'(d) \leq 0$$

undamaged

Def. Phase-Field Functional

$$\Lambda[u, d] \equiv \int_{\Omega} \overset{g(d) \Psi_0(\epsilon)}{\Psi(\epsilon, d)} + G_c \int_{\Omega} \gamma(d, \nabla d)$$

$$- \int_{\Omega} b \cdot u - \int_{\Gamma_f} \bar{f} \cdot u$$

Thm. Euler-Lagrange Eqs

$$\delta \Lambda = 0 \iff \left\{ \begin{array}{l} \textcircled{1} \nabla \cdot b + b = 0, \quad b n = \bar{f} \text{ at } \Gamma_f \\ \textcircled{2} \frac{G_c}{e} (d - \underbrace{\nabla^2 d}_{\parallel}) = -g' \psi_0 \end{array} \right.$$

($\nabla d \cdot n = 0$ on $\partial \Omega$)

pf.

$$\Lambda[u, d] \equiv \int_{\Omega} \underbrace{g(\psi_0)}_{\psi_0} + G_c \int_{\Omega} \underline{\chi(d, \nabla d)}$$

$$- \int_{\Omega} b \cdot \underline{u} - \int_{\Gamma_f} \bar{f} \cdot \underline{u}$$

$$\underline{\delta_u \Lambda = 0} :$$

$$\delta_u \Lambda = \int_{\Omega} \overbrace{g \frac{\partial \psi_0}{\partial \epsilon}}^{=b} : \delta \epsilon - \int_{\Omega} b \cdot \delta u - \int_{\Gamma_f} \bar{f} \cdot \delta u = 0$$

$$\rightarrow \nabla \cdot \mathbf{b} = 0, \quad \mathbf{b} \cdot \mathbf{n} = \bar{t} \text{ on } \Gamma_t$$

$$\underline{\delta_1 \Lambda = 0} :$$

$$\delta_1 \Lambda = \int_{\Omega} \underbrace{g'_\psi}_{\text{par}} \delta \psi + G_c \int_{\Omega} \underline{\underline{\delta \gamma}}$$

$$\delta \gamma = \underbrace{\gamma}_{\frac{d}{2}} \delta \mathbf{d} + \underbrace{\gamma}_{\frac{d}{2}} \underbrace{\delta \nabla \mathbf{d}}_{\text{psd}}$$

$$\gamma = \frac{d^2}{2\ell} + \cancel{\frac{\ell}{2} |\nabla \mathbf{d}|^2}$$

$\nabla \mathbf{d} \cdot \nabla \mathbf{d}$

$$\rightarrow \boxed{\int_{\Omega} \delta \gamma} = \int_{\Omega} \frac{d}{\ell} \delta \mathbf{d} + \int_{\Omega} \underbrace{\ell \nabla \mathbf{d} \cdot \nabla \delta \mathbf{d}}_{\parallel}$$

~~$\int_{\Omega} \nabla \cdot (\ell \nabla \mathbf{d}) \delta \mathbf{d} - \int_{\Omega} \Delta \mathbf{d} \delta \mathbf{d}$~~

~~$\int_{\Omega} \ell \nabla \mathbf{d} \cdot \nabla \delta \mathbf{d}$~~

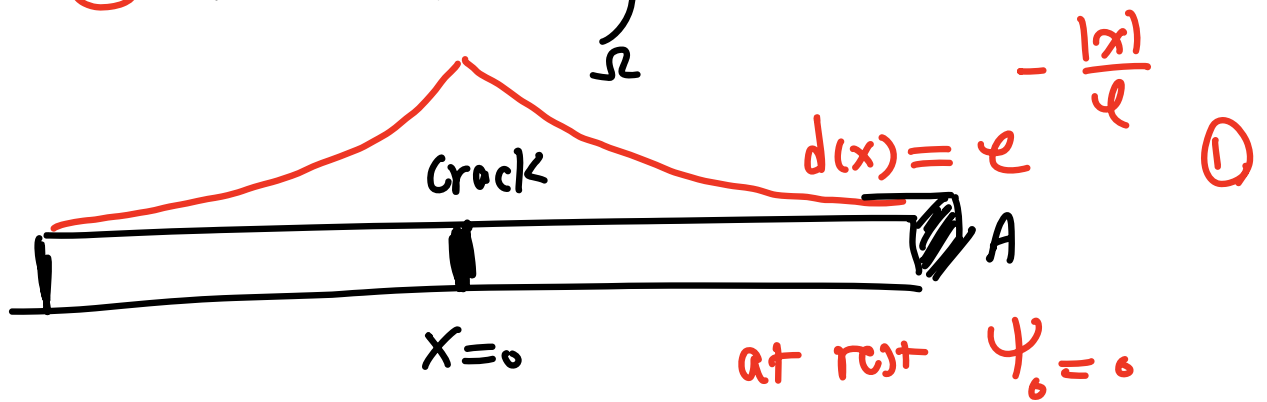
$$\begin{aligned}\delta_1 \Lambda &= \int_{\Omega} g' \psi_0 \delta d + \frac{G_c}{\ell} \int_{\Omega} d \delta d - G_c \int_{\Omega} \Delta d \delta d \\ &= \int_{\Omega} \left(g' \psi_0 + \frac{G_c}{\ell} d - G_c \ell \Delta d \right) \delta d = 0\end{aligned}$$

VPA

□

prop. 1D bar

$$\textcircled{2} \quad A = |\Gamma| = \int_{\Omega} \gamma \, dv$$



pt.

$$\frac{G_c}{\ell} (d - \ell^2 \Delta d) = -g' \psi_0 \rightarrow 0$$

$\Delta d = \frac{d^2}{dx^2}$

$$\rightarrow d - \ell^2 \frac{d^2}{dx^2} = 0 \quad x > 0 \rightarrow d(x) = A e^{\frac{x}{\ell}} + B e^{-\frac{x}{\ell}}$$

$$\rightarrow d(x) = e^{-\frac{|x|}{\ell}}$$

$$\text{at } x \rightarrow \infty \\ d \rightarrow 0$$

$$d(x=0) = 1$$

$$\int_{\Omega} \gamma = \int_A \int_{-\infty}^{+\infty} \gamma = \dots = \int_A dA = A$$

① Crack irreversibility ($\dot{A} \geq 0$)

$$\frac{G_c}{\ell} (d - \ell^2 \Delta d) = - \underline{\underline{g' \Psi_0}} = 2(1-d) \cancel{\Psi_0}^H$$

$g = (1-d)^2$

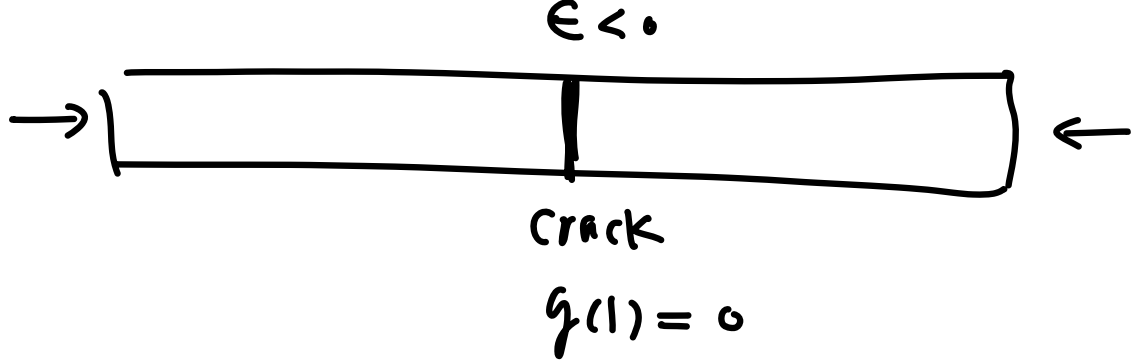
$R =$ resistance to fracture $Y \equiv$ driving force for fracture ($\approx G$)

Replace Ψ_0 with

$$H(x,t) = \max_{s \leq t} \Psi_0(x,s)$$

② Under Compression the sample should not "feel" broken/degraded:

$$\Psi = g(d) \Psi_0 \rightarrow \underline{\underline{G}} = \underline{\underline{g(d) C : \epsilon}}$$



$$\psi_0 = \psi^+ + \psi^-$$

$$\psi = g(l) \psi^+ + \psi^- \rightarrow \delta = g(l) \frac{\partial \psi^+}{\partial \epsilon} + \frac{\partial \psi^-}{\partial \epsilon}$$

Ⓐ Volumetric - Deviatoric Split (isotropic I)

$$\psi_0 = \frac{1}{2} K \epsilon_v^2 + \mu e:e$$

$$\epsilon = \epsilon_v \mathbf{1} + e$$

$$\langle x \rangle_+ = \begin{cases} x & x \geq 0 \\ 0 & x < 0 \end{cases}, \quad \langle x \rangle_- = \begin{cases} 0 & x \geq 0 \\ x & x < 0 \end{cases}$$

$$\psi_0^+ = \frac{K}{2} \langle \epsilon_v \rangle_+^2 + \mu e:e \quad \leftarrow x g(l)$$

$$\psi_0^- = \frac{K}{2} \langle \epsilon_v \rangle_-^2$$

Amor, Marigo, and Maurini (2009)

③ Spectral split

$$\epsilon = \sum_i \epsilon_i \eta_i \otimes \eta_i \rightarrow \epsilon^\pm = \sum_i \langle \epsilon_i \rangle^\pm \eta_i \otimes \eta_i$$

$$\psi_0^\pm = \frac{1}{2} \mathbb{I} \langle \text{tr} \epsilon \rangle_\pm^2 + \mathbb{I} \text{tr}(\epsilon_\pm^2)$$

$$\underline{NB}: \quad \psi_0 = \psi^+ + \psi^- \quad \chi_- \chi_+ = 0$$

Summarize (PFM):

$$\nabla \cdot b + b = 0 \quad \text{on } \Omega, \quad b n = \bar{\epsilon} \quad \text{on } \Gamma_t$$

$$\frac{G_c}{c} (d - c^2 \Delta d) = - \underbrace{g'}_Y \underbrace{H^\psi}_R, \quad H = \max_{s \leq t} \psi_0(x, s)$$

$$\nabla d \cdot n = 0 \quad \text{on } \partial \Omega$$

Thermodynamic perspective:

$$d \geq 0, \quad Y - R \leq 0, \quad d(Y - R) = 0$$

- if $Y < R \longrightarrow \dot{d} = 0$

- if $Y = R \longrightarrow \dot{d} > 0$

$$g = (1-d)^2$$

$$Y = -g' \psi_0 = 2(1-d) \psi_0 \geq 0$$

$$\mathcal{Q} = G \dot{A} \geq 0, \quad \mathcal{Q} = \underbrace{Y}_{\geq 0} \underbrace{\dot{d}}_{\geq 0} \geq 0$$

$$(G, \dot{A}) \sim (Y, \dot{d})$$

$$\frac{d\Lambda}{dA} = -G + G_c \geq 0$$

$$\frac{\delta\Lambda}{\delta d} = -Y + R \geq 0$$

Def.

$$\delta I = \int_{\Sigma} \square \delta d \longrightarrow \square \equiv \frac{\delta I}{\delta d}$$

END of Day 4