

Recap :

$$\left\{ \begin{array}{l} \Psi = \Psi(\epsilon, \dot{\epsilon}, \xi) \\ \sigma = \sigma(\epsilon, \dot{\epsilon}, \xi) \end{array} \right. \xrightarrow{\text{internal vars}} \left\{ \begin{array}{l} \frac{\partial \Psi}{\partial \dot{\epsilon}} = 0 \\ \sigma = \frac{\partial \Psi}{\partial \epsilon} + \underline{\sigma_v} \\ \mathcal{D} = \sigma_v : \dot{\epsilon} + X \cdot \dot{\xi} \geq 0 \end{array} \right. \quad \begin{array}{l} \checkmark \\ \text{viscous stress} \\ \checkmark \end{array}$$

$$\mathcal{D} = \sigma : \dot{\epsilon} - \dot{\Psi} - s\dot{T} - \frac{q \cdot \nabla T}{T} \geq 0$$

$$\dot{\Psi} = \frac{\partial \Psi}{\partial \epsilon} : \dot{\epsilon} + \frac{\partial \Psi}{\partial \dot{\epsilon}} : \ddot{\epsilon} + \frac{\partial \Psi}{\partial \xi} \dot{\xi}$$

$$\left(\frac{\partial \Psi}{\partial \xi} \right) : \dot{\xi} \quad \uparrow \text{Arbitrary Controllable} \\ \neq \dot{\xi}(\text{flux})$$

$$- \frac{\partial \Psi}{\partial \xi} \quad \text{Conjugate force}$$

Def. Dissipation Potential

for the F.J pair, $F = \text{force}$
 $J = \text{flux}$

$$\Phi(J) \geq 0, \Phi(0) = 0, \text{Convex}, F = \frac{\partial \Phi}{\partial J}$$

prop. if F.J contributes to $\mathcal{D}$, and

(F, J) come from $\Phi(J)$ (dissip. potential)

$$\Rightarrow F \cdot J \geq 0$$

Ex: $\mathcal{D} = \underbrace{\sigma_v}_{F} : \underbrace{\dot{\epsilon}}_J + \underbrace{X}_{F} \cdot \underbrace{\dot{\xi}}_J \geq 0$

$$X = - \frac{\partial \Phi}{\partial \xi}$$

$$\frac{\partial \Phi}{\partial \dot{\xi}} = - \frac{\partial \Phi}{\partial \xi}$$

Maxwell-Voigt material

$$\Psi(\epsilon) = \frac{1}{2} \epsilon : \mathbb{C} : \epsilon$$

$$\Phi(\dot{\epsilon}) = \frac{1}{2} \eta \dot{\epsilon} : \dot{\epsilon}$$

no internal var.

$$\mathcal{D} = \sigma_v : \dot{\epsilon} \geq 0$$

$$\sigma = \underbrace{\frac{\partial \Psi}{\partial \epsilon}}_{\mathbb{C} : \epsilon} + \underbrace{\sigma_v}_{\frac{\partial \Phi}{\partial \dot{\epsilon}} = \eta \dot{\epsilon}} \rightarrow \boxed{\sigma = \mathbb{C} : \epsilon + \eta \dot{\epsilon}}$$

Heat Conduction

$$- \underbrace{\frac{q \cdot \nabla T}{T}}_J = \underbrace{q}_{F} \cdot \underbrace{\left(- \frac{\nabla T}{T} \right)}_F \geq 0$$

Def. Quadratic dissipation Potential

$$\Phi(\mathcal{J}) = \frac{1}{2} \mathcal{J} \cdot \overset{\text{tensor/scalar/...}}{\mathcal{M}} \mathcal{J} \quad , \quad \mathcal{M} = \text{positive definite}$$

$$\mathcal{F} = \frac{\partial \Phi}{\partial \mathcal{J}} = \mathcal{M}^{-1} \mathcal{J}$$

$$\rightarrow \boxed{\mathcal{J} = \mathcal{M} \mathcal{F}} \quad \text{linear constitutive law}$$

$$\mathcal{X} \cdot \mathcal{M} \mathcal{X} > 0$$



$$\forall \mathcal{X}$$

$$\mathcal{Y} \cdot \mathcal{M}^{-1} \mathcal{Y} > 0$$

$$\rightarrow \mathcal{F} \cdot \mathcal{J} = \mathcal{F} \cdot \mathcal{M} \mathcal{F} \geq 0$$

entropy producing

Ex: Fourier heat conduction

$$\mathcal{J} = \mathcal{q}$$

$$\mathcal{F} = -\frac{\nabla T}{T}$$

$$\Phi(\mathcal{q}) = \frac{1}{2T} \mathcal{q} \cdot \mathcal{K}^{-1} \mathcal{q}$$

$$-\frac{\nabla T}{T} = \frac{\partial \Phi}{\partial \mathcal{q}} = \frac{1}{T} \mathcal{K}^{-1} \mathcal{q}$$

$$\rightarrow \mathcal{q} = -\mathcal{K} \nabla T \quad \text{familiar}$$

$$g \cdot \left(-\frac{\nabla T}{T} \right) = (-K \nabla T) \cdot \left(-\frac{\nabla T}{T} \right)$$

$$= \frac{\nabla T \cdot K \nabla T}{T} \geq 0 \quad \text{b/c } K \text{ positive definite}$$

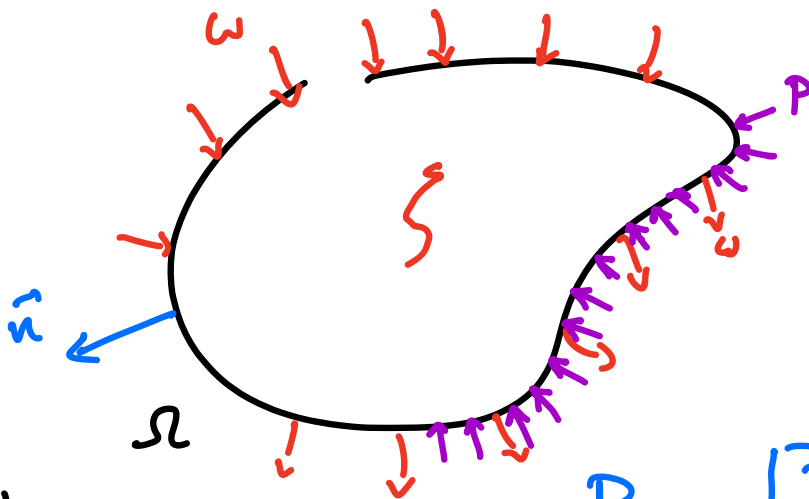
5. Poroelectricity

$$\underbrace{\int}_{\text{fluid content}} \equiv \frac{\text{fluid volume change}}{\text{bulk volume}}$$

$\left. \begin{array}{l} + \\ - \end{array} \right\}$ entering
 exiting

fluid content

Mass balance : $\dot{\int} + \nabla \cdot \omega = 0$



1st law

$$\frac{d}{dt} \int_{\Omega} e \, dv = \cancel{P_{act}} + \dot{Q}$$

$\cancel{P_{ext}} \quad P_{int} = \int_{\Omega} \epsilon : \dot{\epsilon}$

$P_{int} + \boxed{P_{fluid}}$

$$P_{\text{fluid}} = - \int_{\Omega} P n \cdot \omega \, dA = - \int_{\Omega} \underbrace{\nabla \cdot (P \omega)}_{\text{}} \, dV$$

$$\nabla P \cdot \omega + P \underbrace{\nabla \cdot \omega}_{-\dot{\zeta}}$$

$$P_{\text{fluid}} = - \int_{\Omega} (\nabla P \cdot \omega - P \dot{\zeta}) \, dV$$

local form of 4th law

$$\dot{e} = \sigma : \dot{\epsilon} + \underbrace{P \dot{\zeta}}_{\text{}} - \nabla P \cdot \omega - \nabla \cdot q + r$$

Prop. Dissipation inequality

$$\mathcal{D} = \underbrace{\sigma : \dot{\epsilon}}_{\substack{F \\ J}} + \underbrace{P \dot{\zeta}}_{\substack{F \\ J}} - \cancel{\dot{\psi}} - \cancel{s \dot{T}} - \underbrace{\nabla P \cdot \omega}_{\substack{F \\ J}} - \cancel{\frac{q \cdot \nabla T}{T}} \geq 0$$

prop. Porcelain Constitutive law ($T = \omega$)

$$\psi = \psi(\epsilon, \zeta)$$

$$\sigma = \sigma(\epsilon, \xi)$$

$$\rightarrow \dot{\psi} = \frac{\partial \psi}{\partial \epsilon} : \dot{\epsilon} + \frac{\partial \psi}{\partial \xi} \dot{\xi}$$

$$\rightarrow \mathcal{Q} = \underbrace{\left(\sigma - \frac{\partial \psi}{\partial \epsilon} \right)}_{\neq f(\dot{\epsilon})} : \dot{\epsilon} + \underbrace{\left(p - \frac{\partial \psi}{\partial \xi} \right)}_{\neq f(\dot{\xi})} \dot{\xi}$$

$$- \nabla p \cdot \omega \geq 0$$

$$\rightarrow \boxed{\sigma = \frac{\partial \psi}{\partial \epsilon}, \quad p = \frac{\partial \psi}{\partial \xi}, \quad \mathcal{Q} = - \nabla p \cdot \omega \geq 0}$$

$$\frac{\partial \sigma}{\partial \xi} = \frac{\partial p}{\partial \epsilon} = \frac{\partial^2 \psi}{\partial \epsilon \partial \xi}$$

Constitutive law
assumed,
must satisfy
 $\mathcal{Q} \geq 0$

Ex: Biot's free energy

Biot modulus

$$\psi(\epsilon, \xi) = \frac{1}{2} \epsilon : \mathcal{Q} : \epsilon + \frac{1}{2} M (\xi - b \epsilon_v)^2$$

Biot coefficient

$$P = \frac{\partial \psi}{\partial \zeta} = M(\zeta - b \epsilon_v)$$

NB.

$$\frac{\partial \epsilon_v}{\partial \epsilon_{ij}} = 1_{ij}$$

$$\sigma = \frac{\partial \psi}{\partial \epsilon} = \mathbb{C} : \epsilon - \underbrace{b M(\zeta - b \epsilon_v)}_P \mathbb{1}$$

$$\rightarrow \sigma = \mathbb{C} : \epsilon - b P \mathbb{1}$$

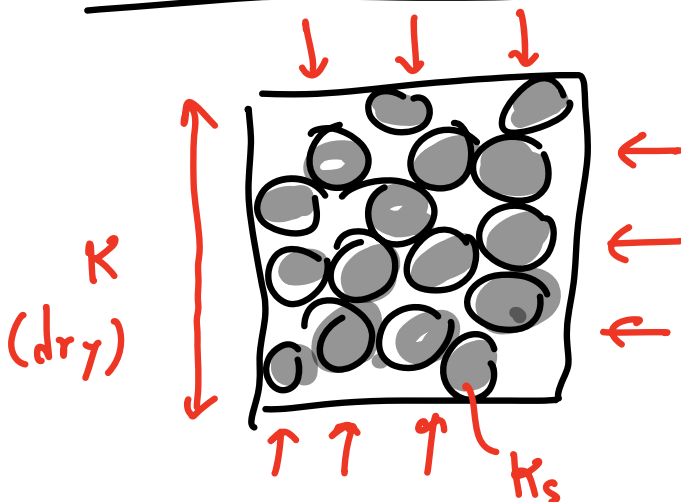
total stress

effective stress

fluid pressure contribution

grain bulk mod.

Relation between (b, M) and (K, K_s)



dry skeleton Bulk modulus

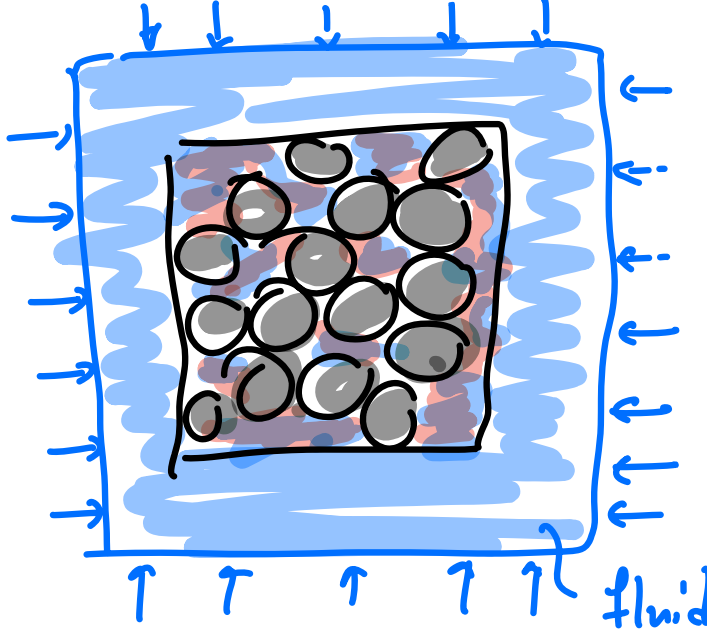
$$K < K_s$$

① Biot coefficient

prop. $b = 1 - \frac{K}{K_s} \leq 1$

soil/loose media $K \ll K_s$
 $\Rightarrow b \simeq 1$

pt.



Consolidated rocks

$$\Rightarrow b < 1$$

unjacketed
Exp.

$$\epsilon_v = - \frac{P}{K_s}$$

$$\frac{\text{tr}}{3} (\sigma = \underline{\underline{C : \epsilon}} - b P \mathbf{1})$$

$$\rightarrow \frac{\text{tr } \sigma}{3} = K \epsilon_v - b P$$

$$-P = \underbrace{\frac{\text{tr } \sigma}{3}}_{\epsilon_m} - \frac{P}{K_s}$$

$$\rightarrow + \cancel{P} = + \frac{K}{K_s} \cancel{P} + \underline{b} \cancel{P}$$

$$\rightarrow \boxed{b = 1 - \frac{K}{K_s}} \quad \square$$

② Biot's Modulus

Let ϕ_f be porosity :

$$\frac{1}{M} = \frac{\phi_f}{K_f} + \frac{b - \phi_f}{K_s}$$

pf.

$$\begin{aligned} \text{① } \left\{ \begin{aligned} \frac{\Delta V_{\text{pore}}}{V_{\text{blk}} V_{\text{pore}}} &= \phi_f \epsilon_v = - \frac{P \phi_f}{K_s} \quad \text{assumption} \\ \frac{\Delta V_{\text{fluid}}}{V_{\text{blk}} V_{\text{pore}}} &= \frac{\Delta V_{\text{fluid}}}{V_{\text{blk}} V_{\text{fluid}}} = - \frac{P \phi_f}{K_f} \end{aligned} \right. \end{aligned}$$

$$\zeta = \frac{P \phi_f}{K_f} - \frac{P \phi_f}{K_s} = P \phi_f \left(\frac{1}{K_f} - \frac{1}{K_s} \right)$$

$$\frac{P}{M} + b \epsilon_v = \frac{P}{K_s}$$

$$P = M (\zeta - b \epsilon_v)$$

Solving for $\frac{1}{M}$, claim is proven. $\square$

Ex:

$$\begin{array}{c} -\cancel{\nabla p} \cdot \omega \\ \swarrow \quad \searrow \\ F \quad \quad \quad \delta \end{array}$$

$$\Phi(\omega) = \frac{\eta_f}{2} \omega \cdot K^{-1} \omega \rightarrow -\nabla \Phi = \frac{\partial \Phi}{\partial \omega} = \eta_f K^{-1} \omega$$

$$\rightarrow \boxed{\omega = -\frac{K}{\eta_f} \nabla p}$$

$$\rightarrow -\nabla p \cdot \omega = \frac{1}{\eta_f} \nabla p \cdot K \nabla p > 0$$

positive def.

Rate-Independent Plasticity ($T = \sigma$)

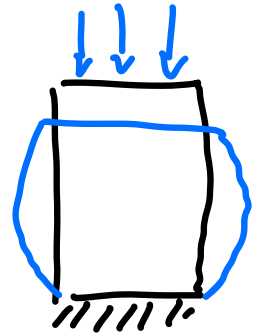
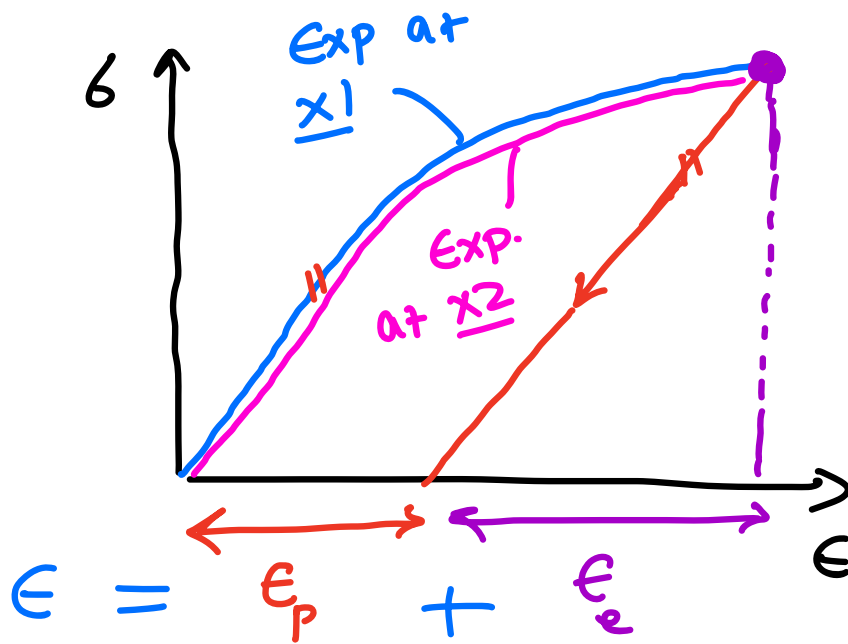
$$\mathcal{D} = \sigma : \dot{\epsilon} - \dot{\psi} \geq 0$$

$$\psi = \psi(\epsilon, \dot{\epsilon}, \xi)$$

$$\sigma = \sigma(\epsilon, \dot{\epsilon}, \xi)$$

$$\rightarrow \sigma = \frac{\partial \psi}{\partial \epsilon} + \dot{\sigma}, \quad \chi = -\frac{\partial \psi}{\partial \xi}$$

$$\mathcal{D} = \cancel{\sigma} : \dot{\epsilon} + X \cdot \dot{\xi} \geq 0$$



For rate-independence :

$$\mathcal{D} = X \cdot \dot{\xi} \geq 0, \quad \sigma = \frac{\partial \psi}{\partial \epsilon}$$

$$\psi = \psi(\epsilon, \xi)$$

$$X = - \frac{\partial \psi}{\partial \xi}$$

$$\sigma = \sigma(\epsilon, \xi)$$

Def. Internal Variables of Plasticity

$$\xi = (\epsilon_p, \alpha)$$

plastic strain tensor

macroscopic + measurable

"hardening" variables

(not measurable)

= microscopic changes

Def. Postulated free energy

$$\Psi(\underline{\epsilon}, \underline{\epsilon}_p, \alpha) = \underbrace{\Psi_e(\underline{\epsilon} - \underline{\epsilon}_p)}_{\substack{\text{reversible} \\ \text{part of free energy}}} + \Psi_h(\alpha)$$

$\underline{\epsilon}_e$ elastic strain

prop. Dissipation inequality

$$\mathcal{D} = \dot{X} \cdot \dot{\xi} \geq 0$$

$$\xi = \begin{pmatrix} \underline{\epsilon}_p \\ \alpha \end{pmatrix} \rightarrow \dot{\xi} = \begin{pmatrix} \dot{\underline{\epsilon}}_p \\ \dot{\alpha} \end{pmatrix}$$

$$X = - \frac{\partial \Psi}{\partial \xi} \rightarrow X = - \begin{pmatrix} \frac{\partial \Psi}{\partial \underline{\epsilon}_p} \\ \frac{\partial \Psi}{\partial \alpha} \end{pmatrix} = \begin{pmatrix} \sigma \\ A \end{pmatrix}$$

$$\rightarrow \begin{cases} \sigma = - \frac{\partial \Psi}{\partial \underline{\epsilon}_p} & \text{macro stress} \\ A = - \frac{\partial \Psi}{\partial \alpha} & \text{"micro stress"} \end{cases}$$

$$\mathcal{D} = \sigma : \dot{\epsilon} - \dot{\psi} \geq 0$$

$$\dot{\epsilon}_e + \dot{\epsilon}_p \quad \frac{\partial \psi}{\partial \epsilon} : \dot{\epsilon}_e + \frac{\partial \psi}{\partial \alpha} \dot{\alpha}$$

$$\mathcal{D} = \left(\sigma - \frac{\partial \psi}{\partial \epsilon_e} \right) : \dot{\epsilon}_e + \sigma : \dot{\epsilon}_p - \frac{\partial \psi}{\partial \alpha} \dot{\alpha} \geq 0$$

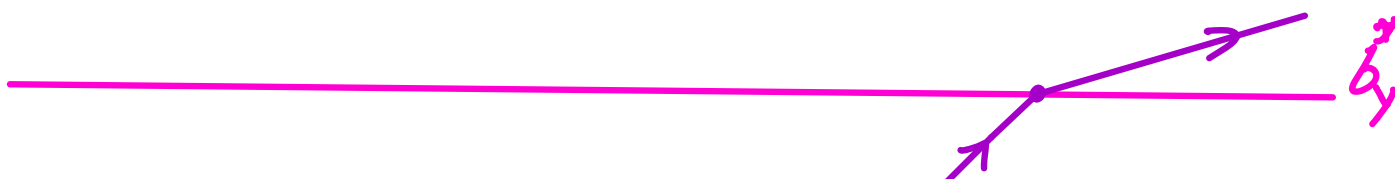
$$\rightarrow \sigma = \frac{\partial \psi}{\partial \epsilon_e} = \frac{\partial \psi_e}{\partial \epsilon_e} = \frac{\partial \psi}{\partial \epsilon_p} \left(\frac{\partial \epsilon_p}{\partial \epsilon_e} \right)$$

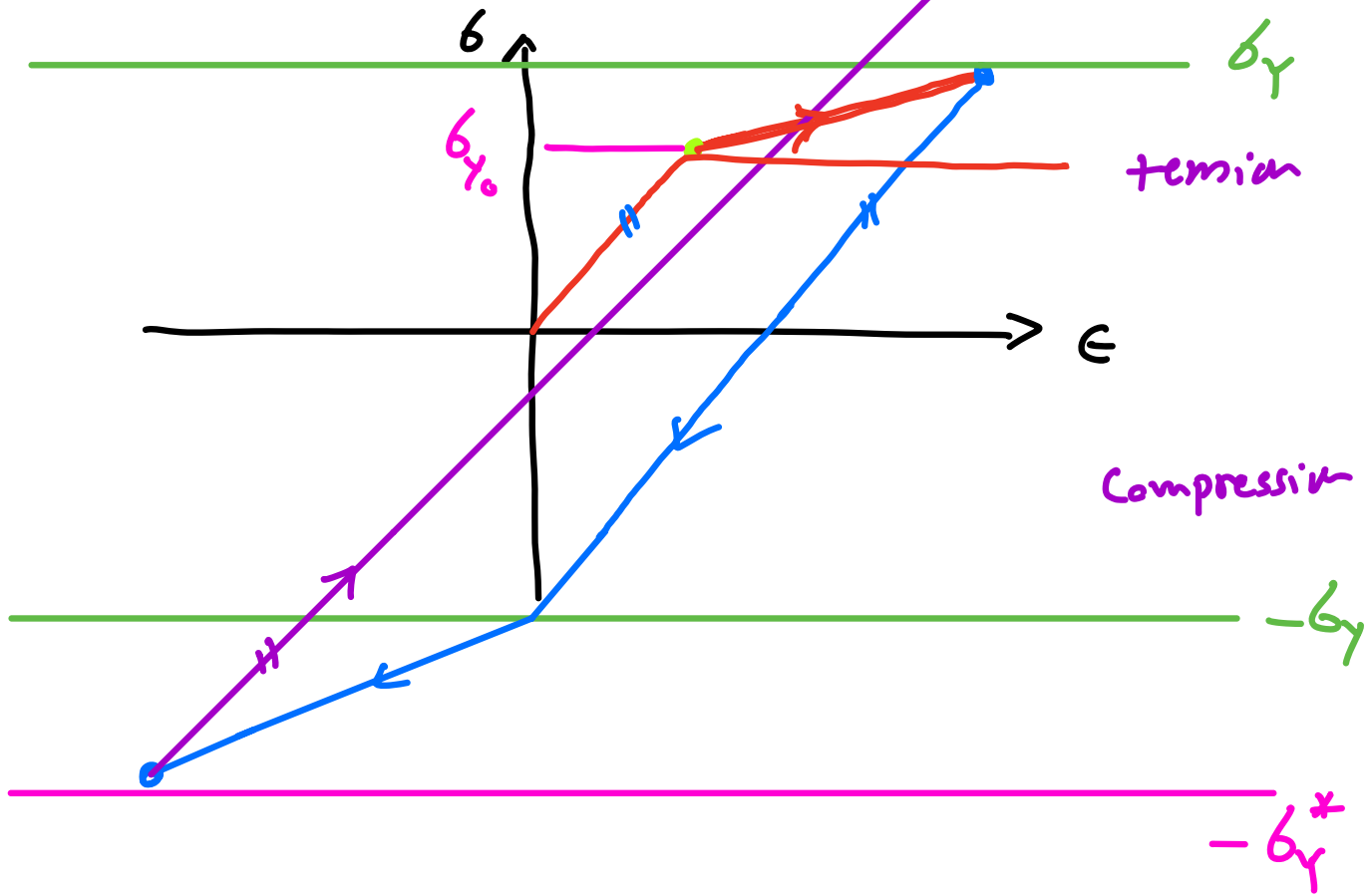
$$= - \frac{\partial \psi}{\partial \epsilon_p}$$

$$\epsilon_p = \epsilon - \epsilon_e$$

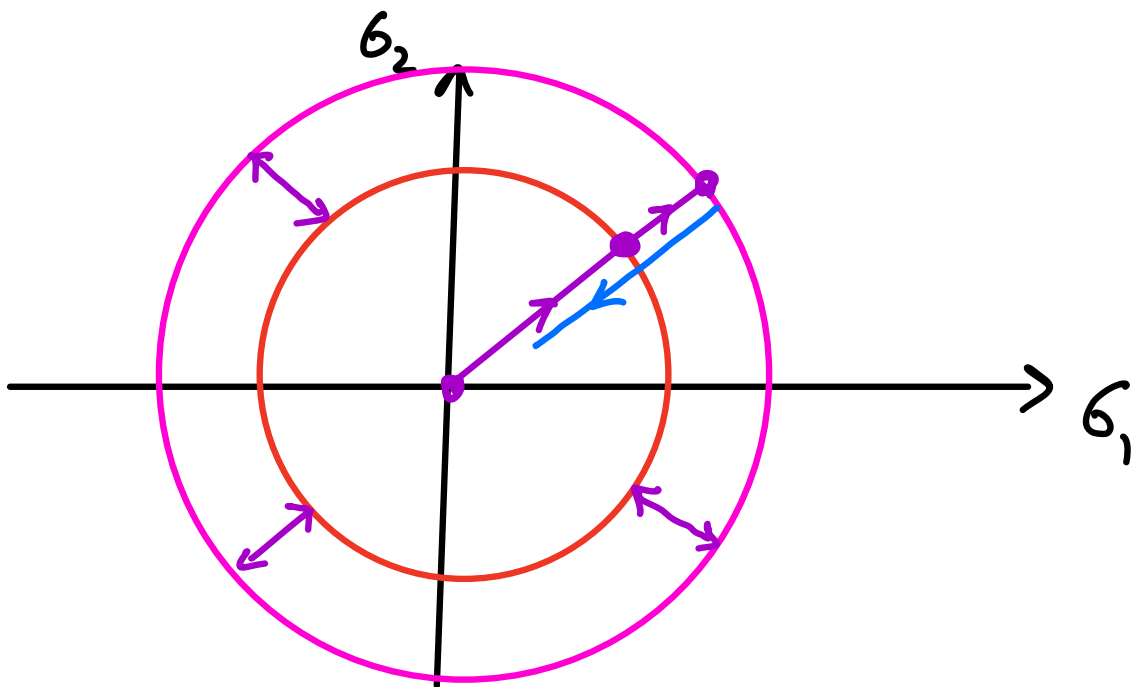
$$\mathcal{D} = \sigma : \dot{\epsilon}_p + A \dot{\alpha} \geq 0$$

dissipation intgr. of plasticity



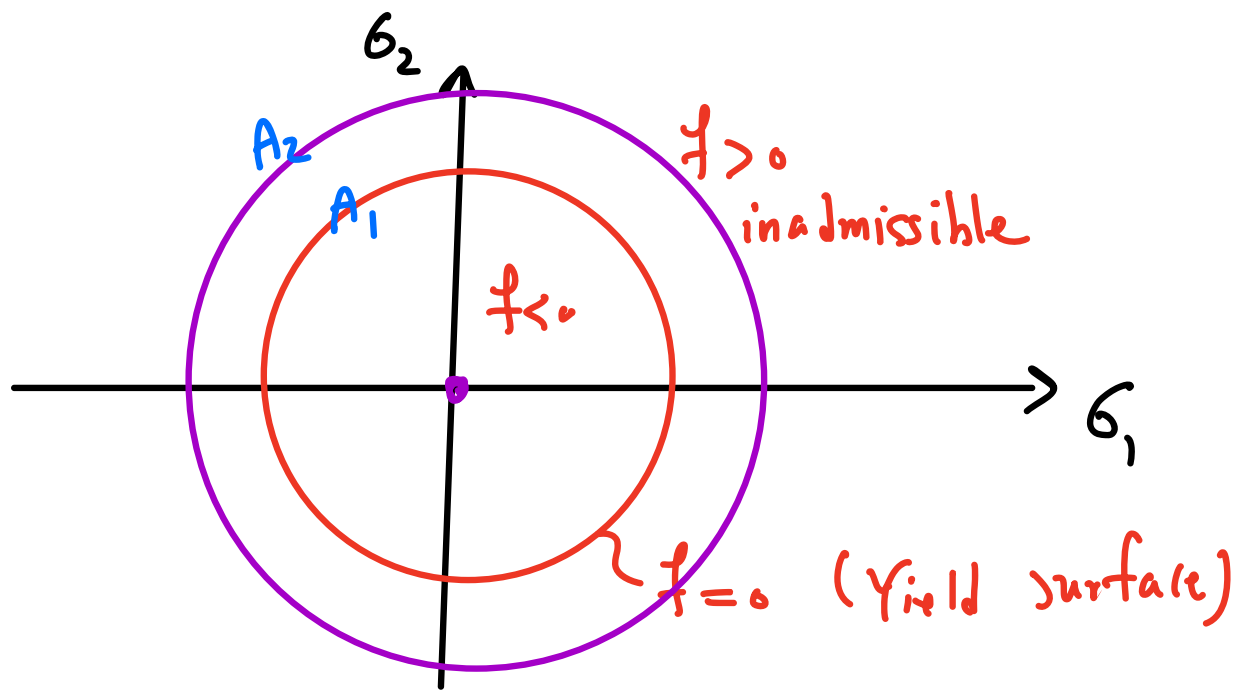


$\sigma \in [-\sigma_Y, \sigma_Y] \equiv E$ elastic region



Def. Yield function and Elastic domain

$f(\sigma, A)$ is called the yield function :



The elastic domain:

$$E = \{ (\sigma, A) \mid f(\sigma, A) \leq 0 \}$$

Dissipation Potential and its problem

Def. $h(cx) = c^n h(x) \quad \forall c > 0$
homogeneous of degree n .

prop. In rate-independent plasticity:

$$D = \sigma : \dot{\epsilon}_p + A \dot{\alpha} = \underbrace{\begin{pmatrix} \sigma \\ A \end{pmatrix}}_{X} * \underbrace{\begin{pmatrix} \dot{\epsilon}_p \\ \dot{\alpha} \end{pmatrix}}_{\dot{\xi}} = X \cdot \dot{\xi} \geq 0$$

The force:

$$X = \frac{\partial \Phi}{\partial \dot{\xi}}$$

$$X(c\dot{\xi}) = X(\dot{\xi}) \quad \forall c > 0$$

homogeneous of degree zero.

Claim:

$$\Phi(c\dot{\xi}) = c \Phi(\dot{\xi})$$

homogeneous of degree one.

+ not differentiable at $\dot{\xi} = 0$

pf.

$$h(c) \equiv \Phi(c\dot{\xi})$$

$$h'(c) = \dot{\xi} \underbrace{\frac{\partial \Phi}{\partial \dot{\xi}}(c\dot{\xi})}_{X(c\dot{\xi})} = \dot{\xi} \underbrace{X(c\dot{\xi})}_{X(\dot{\xi})}$$

$$\rightarrow h'(c) = \dot{\xi} X(\dot{\xi}) \xrightarrow{\int dc} h(c) = c \dot{\xi} X(\dot{\xi})$$

$\downarrow$
 $h(0) = \Phi(0) = 0$

$$\rightarrow \boxed{\Phi(c\dot{\xi}) = c \dot{\xi} X(\dot{\xi}) = c \Phi(\dot{\xi})}$$

$$c=1 \rightarrow \underline{\Phi(\dot{\xi})} = \dot{\xi} X(\dot{\xi})$$

Φ is hom.
of degree 1

$$\Phi(\underset{c\dot{\xi}}{y}) = \cancel{\Phi(0)} + \underbrace{\frac{\partial \Phi}{\partial \dot{\xi}}(0)}_{X_0} (y - 0) + o(y^2)$$

$$\rightarrow \underbrace{\frac{\Phi(c\dot{\xi})}{c}}_{\Phi(\dot{\xi})} = \cancel{c} X_0 \cdot \dot{\xi} + \frac{o(c^2)}{\cancel{c}} \quad \lim_{c \rightarrow 0}$$

$$\rightarrow \Phi(\dot{\xi}) = X_0 \cdot \dot{\xi}$$

↪ linearity &
 $\Phi(\dot{\xi}) \geq 0 \quad \forall \dot{\xi}$
in compatible
□

Ex: 1D bar



Assume no hardening var:

$$\mathcal{D} = \epsilon : \dot{\epsilon}_p \geq 0$$

$$\Phi(\dot{\epsilon}_p) = \begin{cases} \dot{\epsilon}_p \Phi(1) & \dot{\epsilon}_p \geq 0 \\ |\dot{\epsilon}_p| \Phi(-1) & \dot{\epsilon}_p < 0 \end{cases}$$

$$\dot{\epsilon}_p \geq 0$$

$$\dot{\epsilon}_p < 0$$

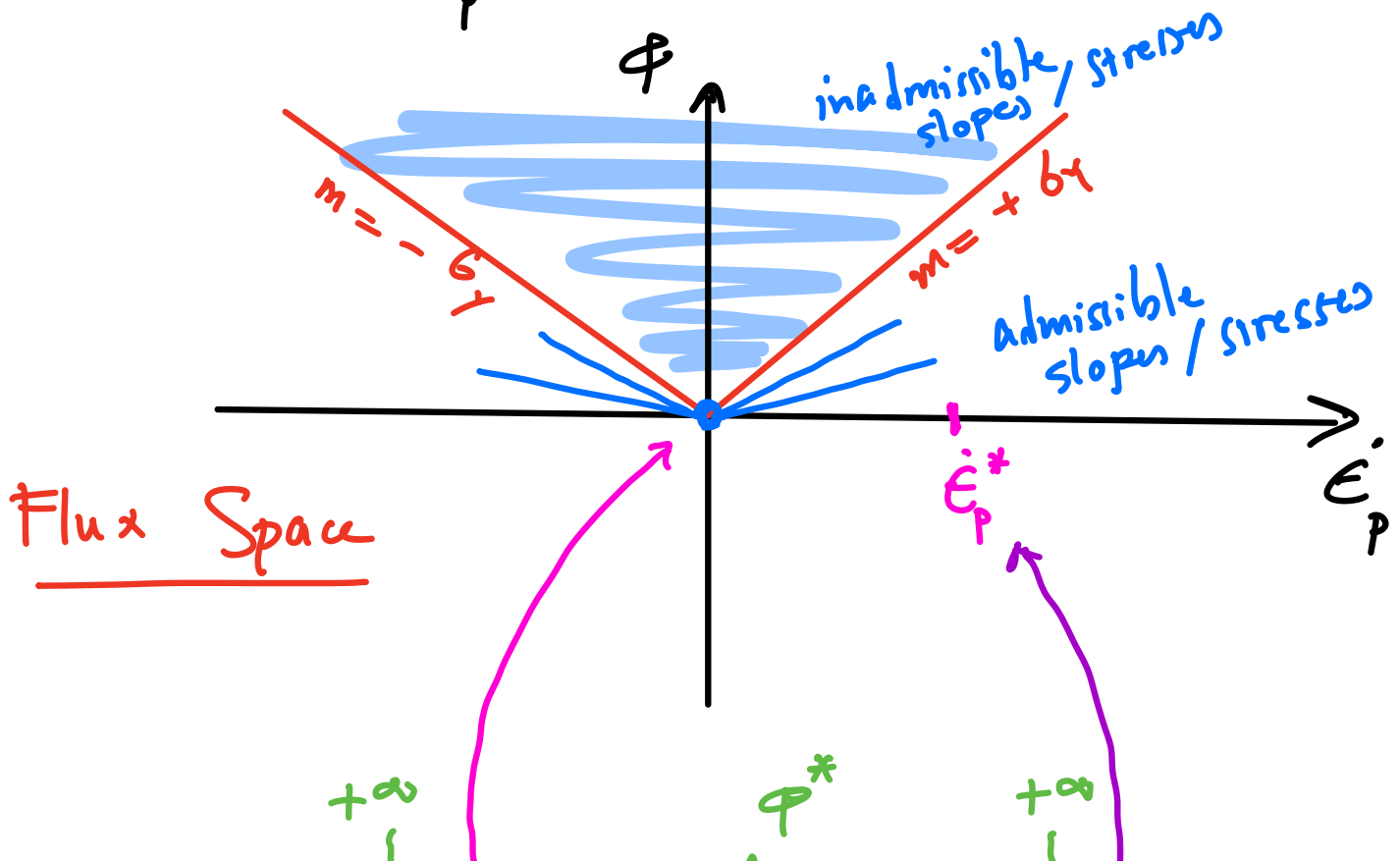
hom of
deg. 1

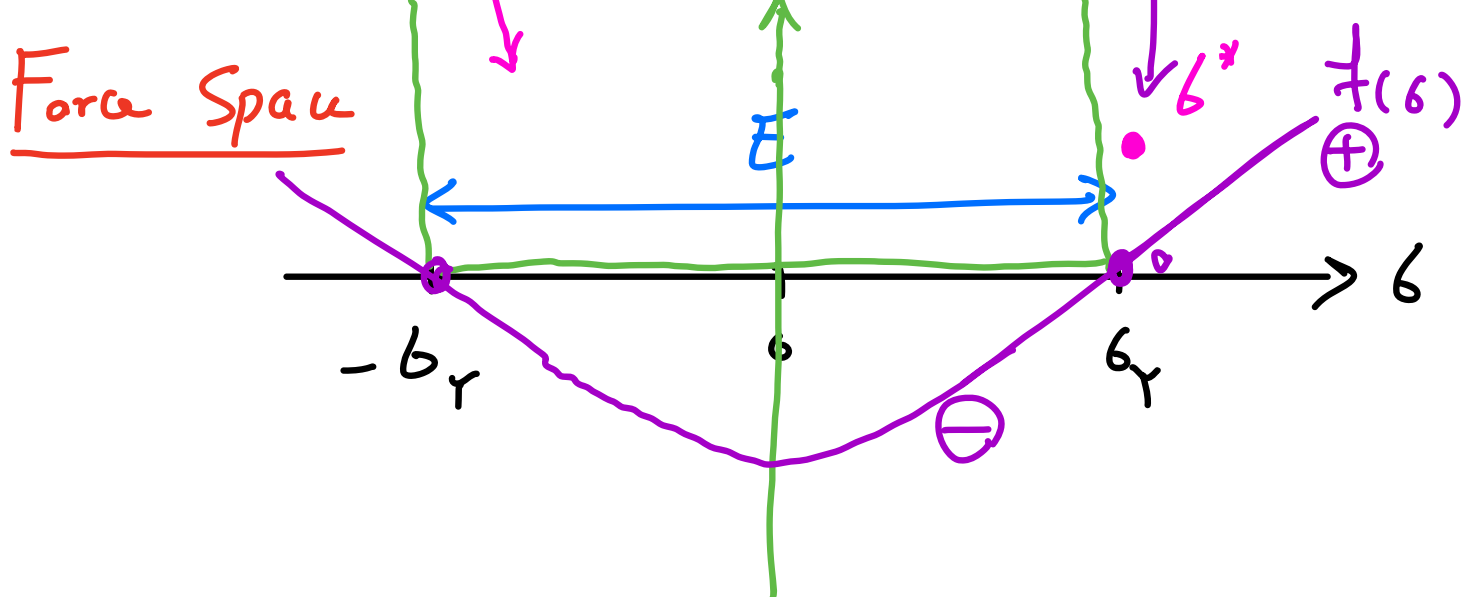
Assume



$$\Phi(\dot{\epsilon}_p) = \sigma_y |\dot{\epsilon}_p|$$

$$\Phi(1) = \Phi(-1) = \sigma_y$$





$$\Phi^*(x) \equiv \max_{\dot{\xi}} \{ x \cdot \dot{\xi} - \Phi(\dot{\xi}) \}$$

$$\dot{\xi} = \frac{\partial \Phi^*}{\partial x}$$

Def. Internal variables evolve according to the following flow rules:

mag. of flow

$$\dot{\epsilon}_p = \dot{\gamma} \left(\frac{\partial g}{\partial b} \right), \quad \dot{\alpha} = \dot{\gamma} \left(\frac{\partial g}{\partial A} \right)$$

plastic multiplier ($\dot{\gamma} \geq 0$)

direction of flow

where $g(b, A)$ is plastic potential.

Flow must be subject to:

$$\dot{\gamma} \geq 0, \quad f \leq 0, \quad \dot{\gamma}f = 0$$

Karush - Kuhn - Tucker (KKT) conditions.

$$\textcircled{1} \quad \dot{\gamma} = 0 \rightarrow \dot{\epsilon}_p = 0, \quad \dot{\alpha} = 0, \quad f < 0$$

deformation is elastic

$$\textcircled{2} \quad \dot{\gamma} > 0 \rightarrow f = 0$$

deformation is plastic
 $\dot{\epsilon}_p \neq 0, \quad \dot{\alpha} \neq 0$

Def. if $g = f \Rightarrow$ associative flow rule (metal, —)

if $g \neq f \Rightarrow$ non-associative (rocks, soil)

prop. Associative flow satisfies $D \geq 0$

Assume
 $f(x)$ is
convex

$$D = \sigma : \dot{\epsilon}_p + A \dot{\alpha} \geq 0 \rightarrow D = X \cdot \dot{\gamma} \geq 0$$

(pf. if $\dot{\gamma} = 0 \rightarrow \dot{\epsilon}_p = 0, \quad \dot{\alpha} = 0 \rightarrow D = 0$ ✓)

$f(x) \leq 0$ if $\dot{\gamma} > 0 \rightarrow f(x) = 0$

$$(D = \dot{\gamma} X \frac{\partial f}{\partial x} \geq 0 \quad \checkmark \quad \text{target})$$

$$0 \geq \cancel{f(y)} \geq \cancel{f(x)} + \frac{\partial f}{\partial x} (\cancel{y} - x)$$

$$\rightarrow x \cdot \frac{\partial f}{\partial x} \geq 0$$

□

prop. flow rule + KKT $\Rightarrow$ rate independence

P.P. $\hat{\epsilon}_p(t) \equiv \epsilon_p(ct) \quad c > 0$

$$\boxed{\dot{\hat{\epsilon}}_p = c \dot{\epsilon}_p(ct) = \underbrace{c \dot{\gamma}}_{\dot{\gamma}} \frac{\partial g}{\partial b}}$$

Thm. Maximum dissipation Principle

Given any $(\dot{\epsilon}_p, \dot{\alpha})$ and (b, A) , the following are equivalent: admissible

① $x \cdot \dot{\epsilon} \geq x^* \cdot \dot{\epsilon} \quad \forall x^*, \quad f(x^*) \leq 0$

② flow is associative ($f=g$):

$$\dot{\xi} = \dot{\gamma} \frac{\partial f}{\partial \dot{b}}, \quad \dot{\gamma} \geq 0, \quad \dot{\gamma} f(x) = 0$$

pf. in the notes.

Corollary. Maximum Dissipation Principle (MDP)

$$\Rightarrow \mathcal{D} = X \cdot \dot{\xi} \geq 0$$

pf. $\mathcal{D} = X \cdot \dot{\xi} \geq \cancel{X^* \cdot \dot{\xi}} \quad \forall X^*$

pick $X^* = 0$

□

Remark. MDP allow defining $\Phi(\dot{\xi})$

$$\Phi(\dot{\xi}) \equiv \max_{f(x^*) \leq 0} X^* \cdot \dot{\xi} \quad \stackrel{\exists X}{=} X \cdot \dot{\xi}$$

~~$X = \frac{\partial \Phi}{\partial \dot{\xi}}$~~ $X \in \partial \Phi$

3. Consistency Condition $\Rightarrow \dot{\gamma}$

$$\dot{\epsilon}_p = \dot{\gamma} \frac{\partial g}{\partial \dot{b}}, \quad \dot{\alpha} = \dot{\gamma} \frac{\partial g}{\partial \dot{A}}$$

how to
compute

During flow $f(x) = 0 \rightarrow \dot{f} = 0$

$$\frac{d}{dt} f(b, A) = \frac{\partial f}{\partial b} : \dot{b} + \frac{\partial f}{\partial A} \dot{A} = 0$$

$\downarrow$ $\checkmark$ $\downarrow$?

$$\dot{b} = \frac{d}{dt} \mathbb{C} : \epsilon_e = \mathbb{C} : \dot{\epsilon}_e$$

$$b = \frac{\partial \psi_e}{\partial \epsilon_e}$$

$$\dot{A} = - \frac{\partial^2 \psi_h}{\partial \alpha^2}$$

$$= - \frac{\partial^2 \psi_h}{\partial \alpha^2} \dot{\alpha} \quad \dot{\gamma} \frac{\partial g}{\partial b} \quad \dot{\gamma} \frac{\partial g}{\partial A}$$

$$\dot{b} = \left(\frac{\partial^2 \psi}{\partial \epsilon_e^2} \right) : \dot{\epsilon}_e$$

$(\dot{\epsilon} - \dot{\epsilon}_p)$
 $\dot{\gamma} \frac{\partial g}{\partial b}$

$$\rightarrow \frac{\partial f}{\partial b} : \mathbb{C} : \left(\dot{\epsilon} - \dot{\gamma} \frac{\partial g}{\partial b} \right)$$

$$- \frac{\partial f}{\partial A} \frac{\partial^2 \psi_h}{\partial \alpha^2} \frac{\partial g}{\partial A} \dot{\gamma} = 0$$

$$\dot{\gamma} = \frac{\frac{\partial f}{\partial \dot{\epsilon}} : \dot{\epsilon} : \dot{\epsilon}}{\frac{\partial f}{\partial \dot{\epsilon}} : \dot{\epsilon} : \frac{\partial \dot{\gamma}}{\partial \dot{\epsilon}} + \frac{\partial f}{\partial A} \frac{d^2 \psi_h}{d\alpha^2} \frac{\partial \dot{\gamma}}{\partial A}}$$

$\equiv H$ hardening modulus

END of Day 3